

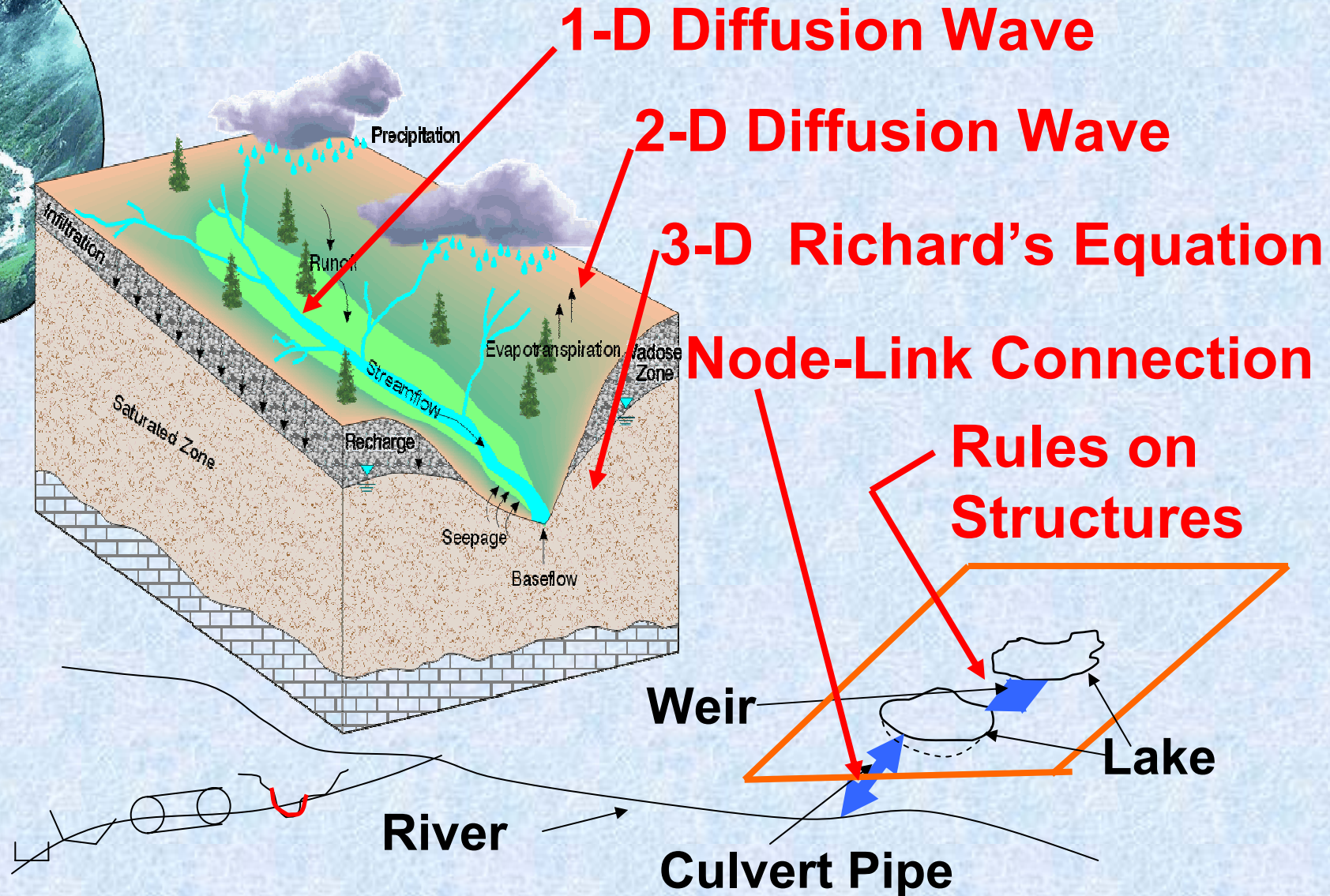
# **Kissimmee Watershed Planning and Operations Project**

## **Model Evaluation for MODHMS**

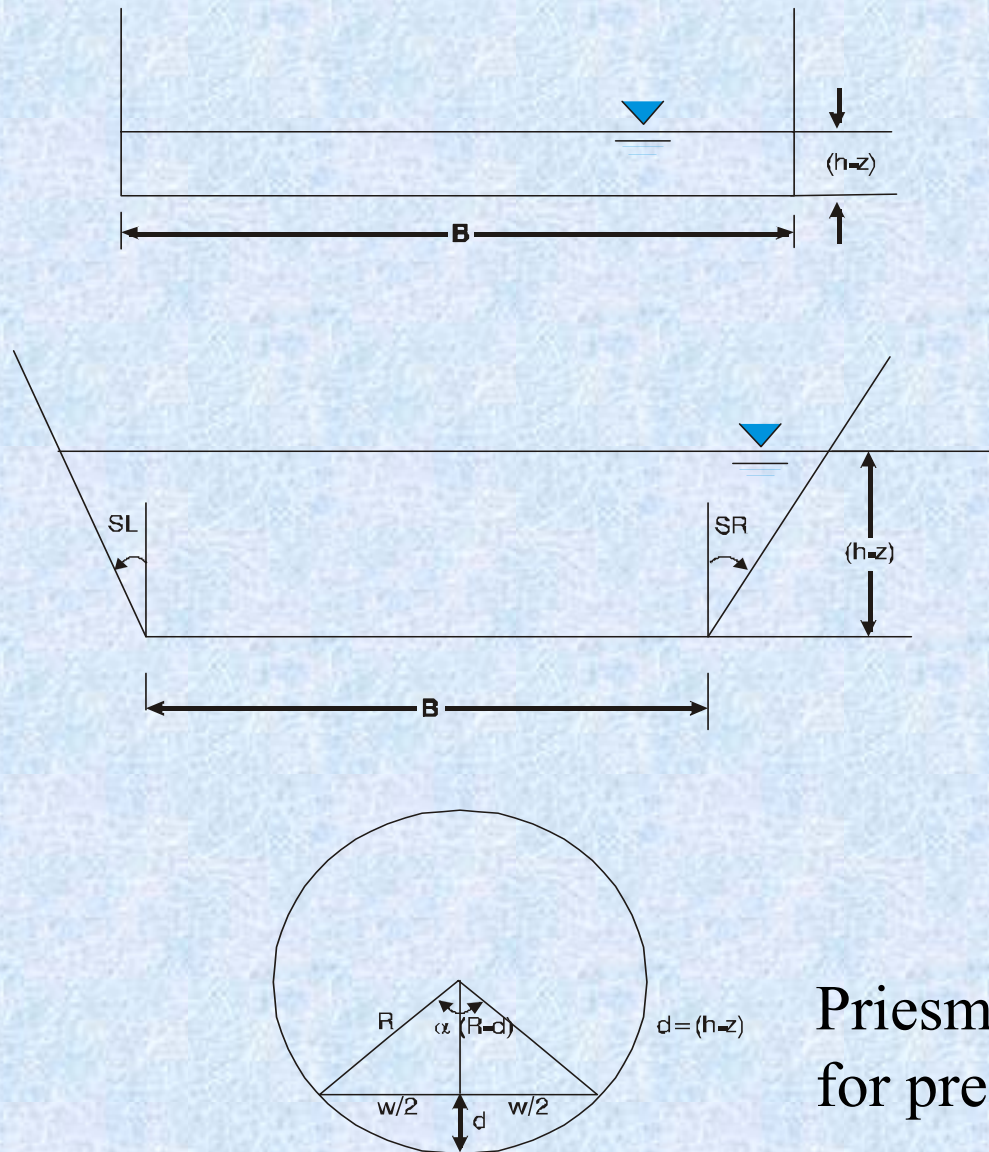
**Sorab Panday, Joe Hughes**



# Governing Equations



# Special Channel Section Types



Priesmann slot concept  
for pressurized flow



# Hydraulic Structures Simulation Capability

## CULVERTS:



### Designs:

- Box
- Pipe
- Embedded
- Countersunk
- With Weirs/baffles
- Arrayed
- Inlet/Outlet drops

## GATES:



## WEIRS:



### Designs:

- Rectangular
- Triangular
- Notched
- Finger Weirs

## REGULATING STRUCTURES:

$$Q = Q(t)$$

$$Q = f(\text{distant flow})$$

$$Q = f(\text{distant head})$$

Pump Stations

Other Structures

# Hydraulic Structure Computation

General hydraulic structure computational schemes are provided by supplying various stage-discharge relations (observed or computed):

$Q$  is a function of  $h_{\text{ups}}$

$Q$  is a function of  $h_1, h_2$

$Q$  is a function of  $h_{\text{ups}}, h_{\text{dns}}$

$Q = Q_1 + Q_2$  where

$Q_1 = f(h_1)$  and  $Q_2 = f(h_2)$

Need tabular values of  $h_1$ ,  $(h_1 - h_2)$ , and  $Q$  to ensure that  $Q = 0$  when  $h_1 = h_2$ .

Flux	H1 = 1	H1 = 5	H1 = 10
H2 = 0	10	50	100
H2 = 1	0	30	70
H2 = 2	-10	10	40

For  $H1 = 1$  and  $H2 = 1$ , the flux is zero

For  $H1 = 2$  and  $H2 = 2$ , the flux is -5

For  $H1 = 1.5$  and  $H2 = 1.5$ , the flux is -1.875

# Regulation of Structures

- Unregulated and regulated structures can be present in a simulation
- Unregulated structures are always on
- Regulated structures are operated according to a set of rules
- Two types of rules
  - Operation Rules
  - Shift-work Rules



# Operation Rules

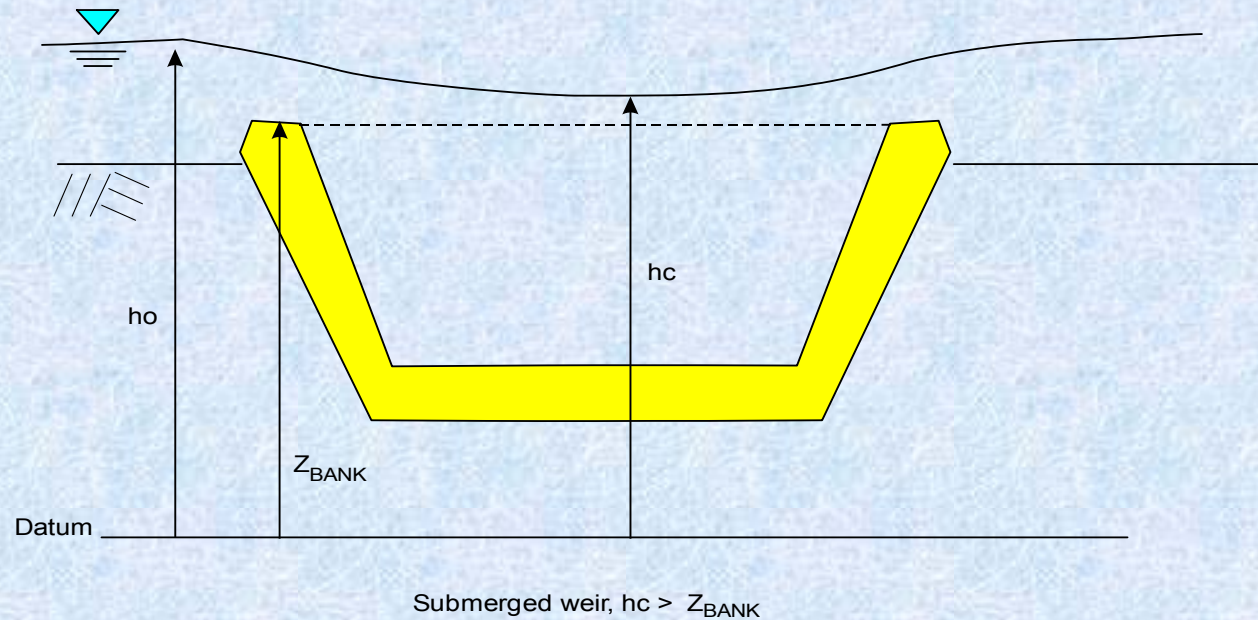
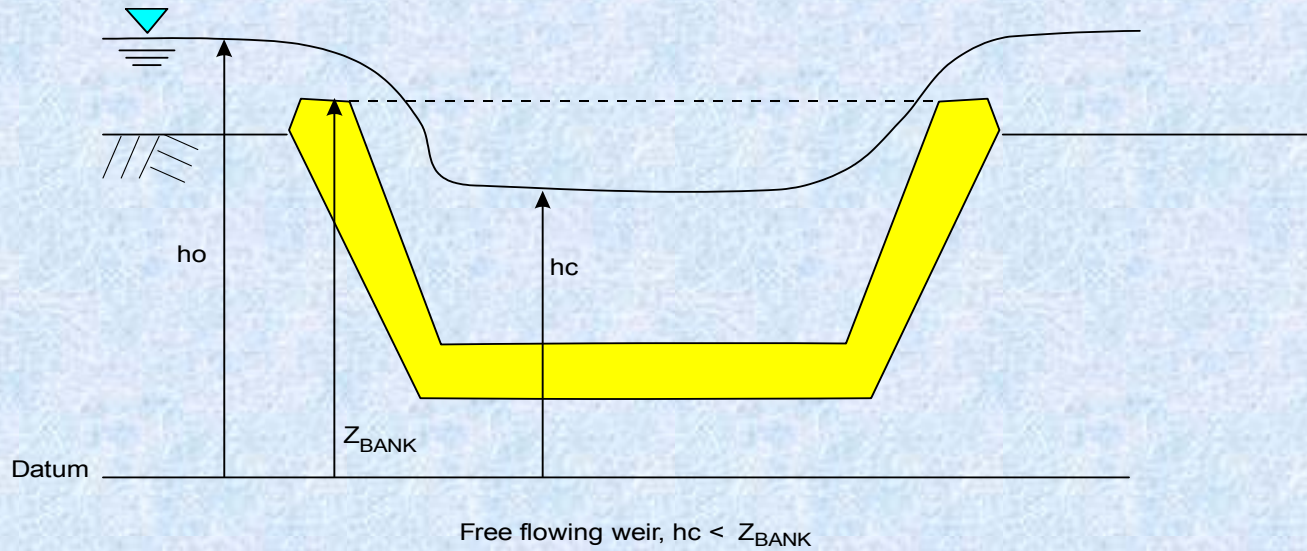
- A structure may **OPEN / CLOSE** if the **HEAD / FLUX** at a trigger location (in GW, OLF, or CHF domain) is **ABOVE / BELOW** a trigger value and within times ( $T_{start}$ ,  $T_{end}$ ).
- A **two-way** trigger: If structure opens above a trigger value, it also closes below trigger value.
- Structure subject to a **maximum flow** rate
- Multiple (**independent** or **dependent**) rules for operating a structure
- Trigger subject to **relative difference** between heads or flows at two locations



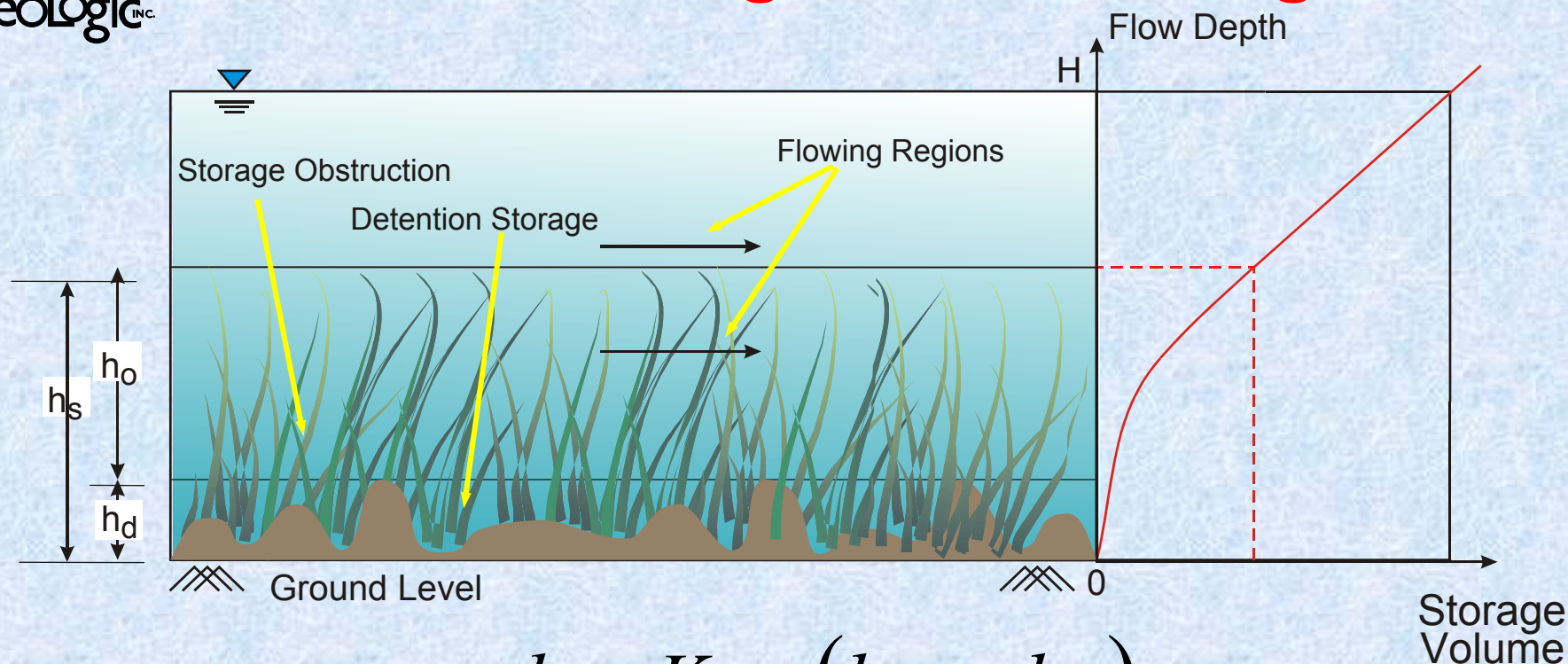
# Shift-work Rules

- During a cyclic period (24 hours), shift-work occurs between  $T_{\text{start\_shift}}$  (9 hours) and  $T_{\text{end\_shift}}$  (18 hours) when within times ( $T_{\text{start}}$ ,  $T_{\text{end}}$ ).
- Structure is operated only during period of shift-work.
- Two options when outside of shift period
  - Structure is always off outside of shift period
  - Structure is maintained in it's on/off state outside of shift period

# Channel - Overland Flow Interaction



# Surface Storage and Exchange Terms



$$q_{go} = k_{rgo} K_{GO} (h_G - h_o)$$

- $k_{rgo}(h_{ups}) = 0$  at land surface; 1 at top of rills
- Horizontal flow above height  $h_d$
- Horizontal flow obstruction option

# Groundwater Interaction Fluxes

Overland - Groundwater flow

$$q_{go} = k_{rvo} K_{GO} (h_G - h_O) = Q_{go} / (\Delta x \Delta y)$$

Channel - Groundwater flow

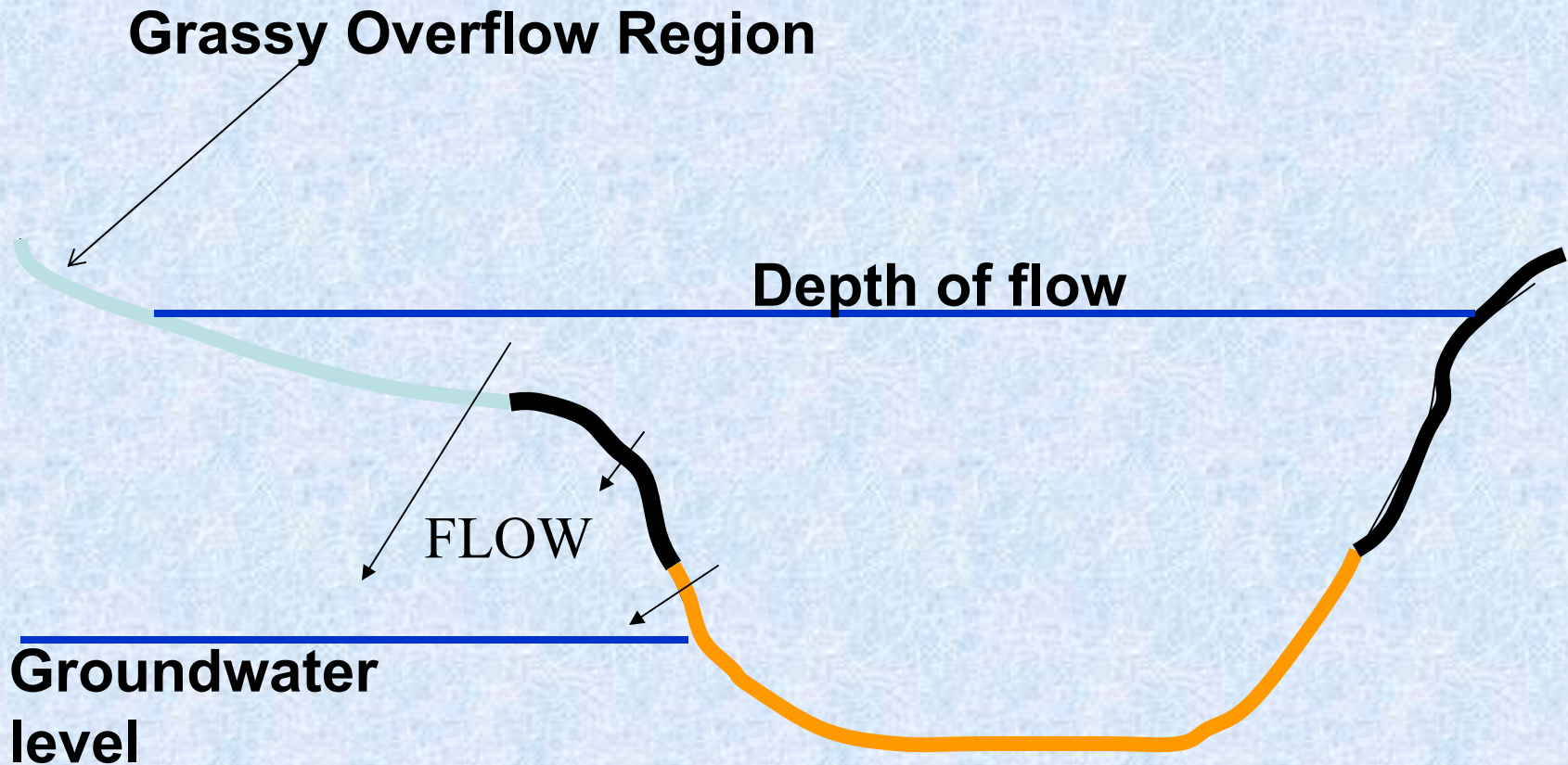
$$q_{gc} = k_{rvc} K_{GC} (h_G - h_C) = Q_{gc} / L P_{ups}$$

where  $K_{GC}$  may be a constant or vary with flow depth.  
For varying  $K_{GC}$  with conductivity  $K_I$  to depth  $d_I$  etc.

$$K_{eff} (Y_1) = \frac{K_1 P_1 + K_2 (P_2 - P_1) + K_3 (P(Y_1) - P_2)}{P(Y_1)}$$

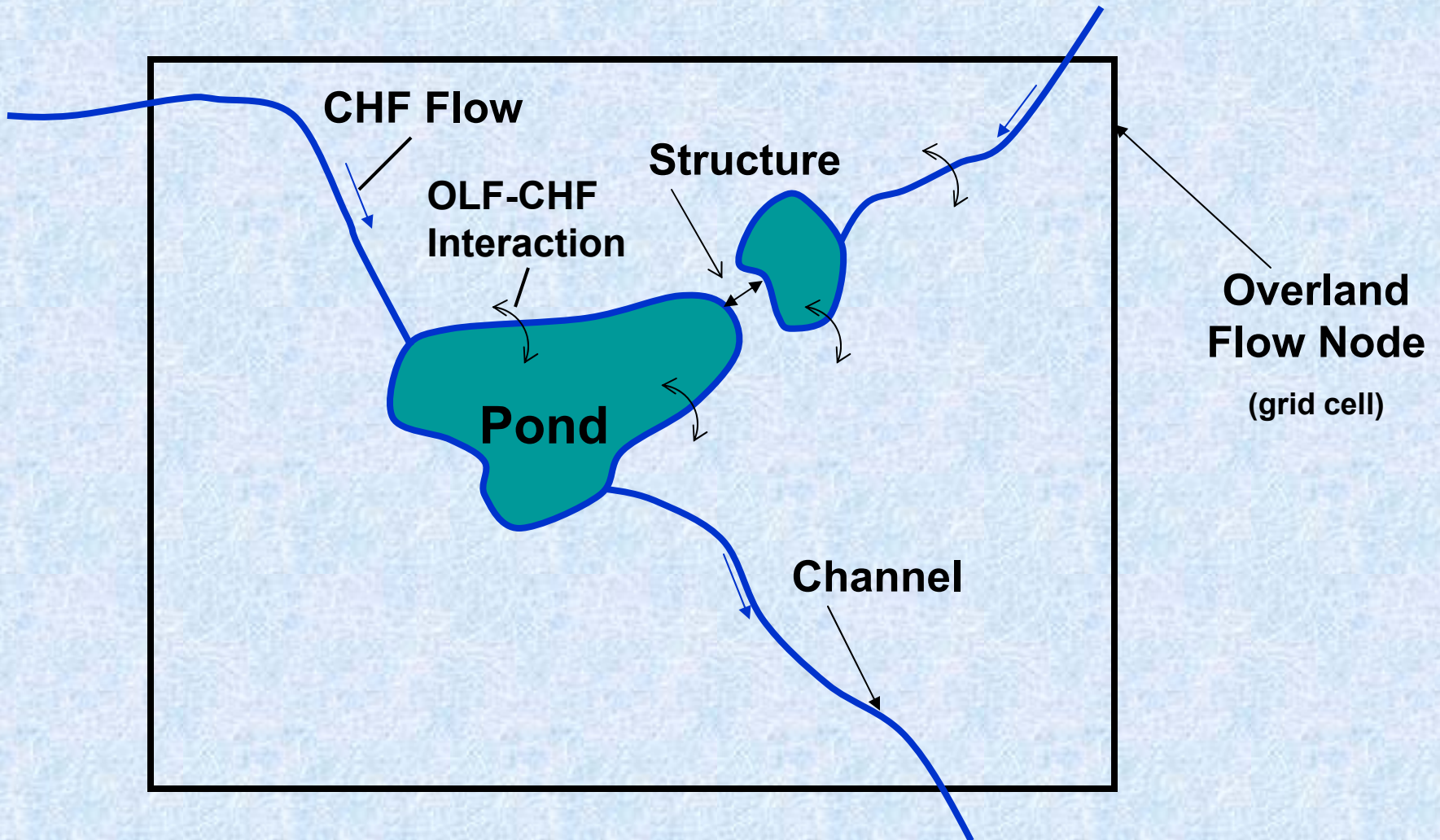


# Leakance varying with depth of flow within Channel Section



$$K_{eff} (Y_1) = \frac{K_1 P_1 + K_2 (P_2 - P_1) + K_3 (P(Y_1) - P_2)}{P(Y_1)}$$

# Small Surface Water Bodies



# Small Surface-Water Bodies

- A channel node represents a surface-water body
- Tabular stage-area relationship for the surface-water body provides:
  - Storage term computation
  - Area over which groundwater connection occurs
  - Effective leakance computation for varying leakance with flow-depth
- Perimeter of surface-water body provides length over which overland connection occurs
- Direct connection to channel node
- Connection to other surface-water body via a structure

## Direct Flow Links between Nodes

- Connect isolated parts of a domain using a variety of Q-h relationships
- Links can be made between any nodal component (GW, OLF, CHF, and stage-storage nodes)
- A structure formula provides flow in the link (various tabulated Q-h relationships)
- Channel flow equations and all cross-section types also included for links (with storage and OLF / GW interactions)



# Other Hydrologic Components

- Interception Storage (bucket model)
- Evapotranspiration
  - **Physics based and Parametric options**
  - **PET may be input or calculated. Calculated methods include:**
    - **Bare Ground (Senarath et al., WRR 36,3, 2000)**
    - **Vegetated Surfaces (Penman Montieth)**
- Infiltration formulas – Kostiaikov; Green Ampt; GSVE
- All water features and boundary conditions available in MODFLOW – HFB, FHB, CHD, GHB, OBS extended to OLF and CHF domains
- Recharge Time-Series (RTS) for short-term events
- Reactive Transport capability for all domains

# Interception & Evapotranspiration

- **Bucket Model for Interception**
  - Interception storage =  $f(LAI)$
  - Recharge to ground after interception is full
  - $ET_{ref}$  first met from interception storage
  - Remaining ET from transpiration & evaporation
- **Physics-based Evapotranspiration varies with:**
  - LAI (transient input)
  - Moisture Content (state variable)
  - Root Zone Distribution Function / Evaporation Distribution Function (transient input)
- **Parameteric Evapotranspiration**
  - ET flux varies with depth to water table

# Adaptive Time-Stepping

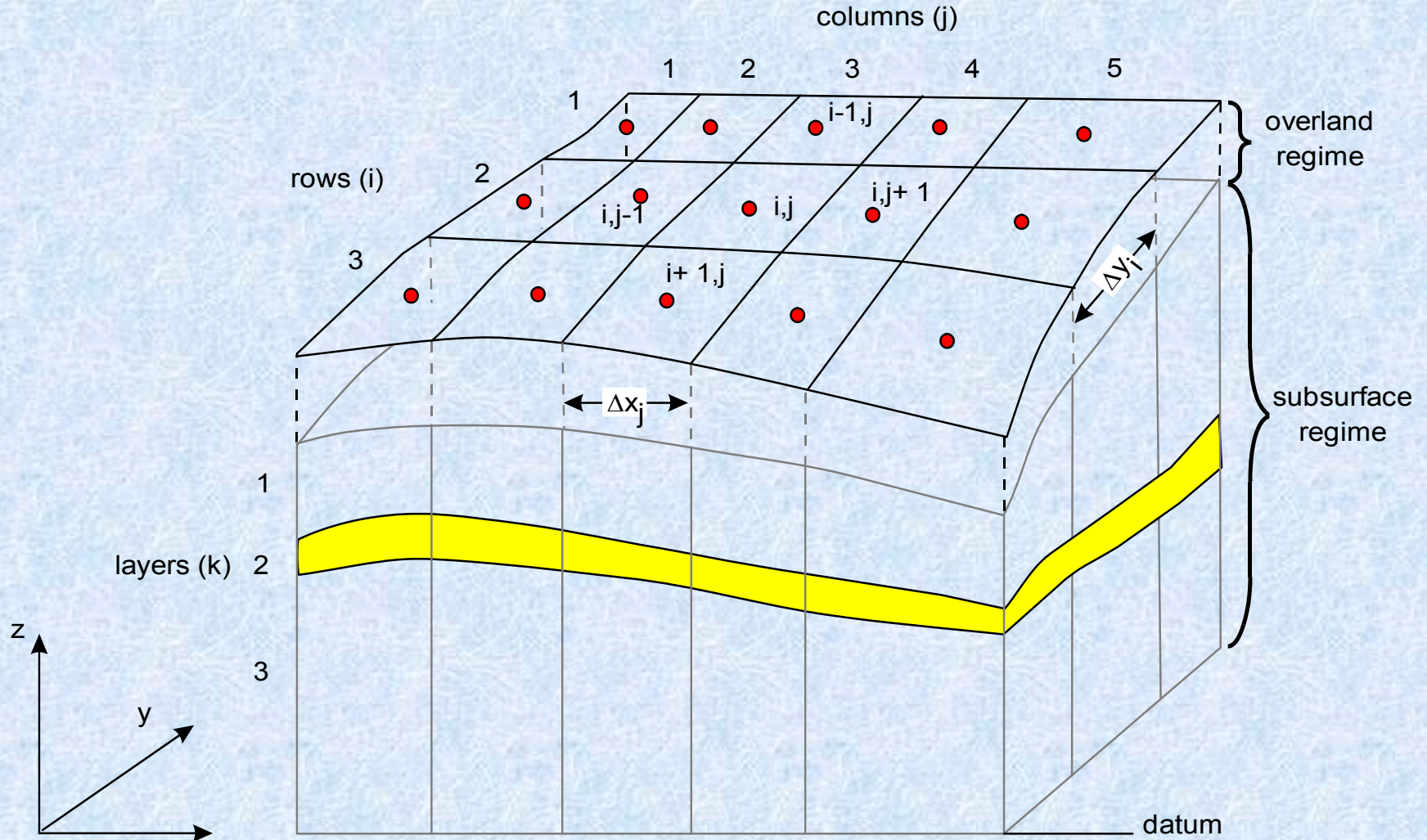
- For short-term events, utilize refined computational time steps adapted to lie exactly at start and end times of rainfall events (and optionally for rule changes)
- Within hiatus periods, time-step sizes increase depending on problem non-linearity
- Time steps also adapted to accommodate printing times supplied by user
- Averaged hyetographs may be provided for long-term simulations
- Option for restart at non-zero relative time

# Time-varying Conditions

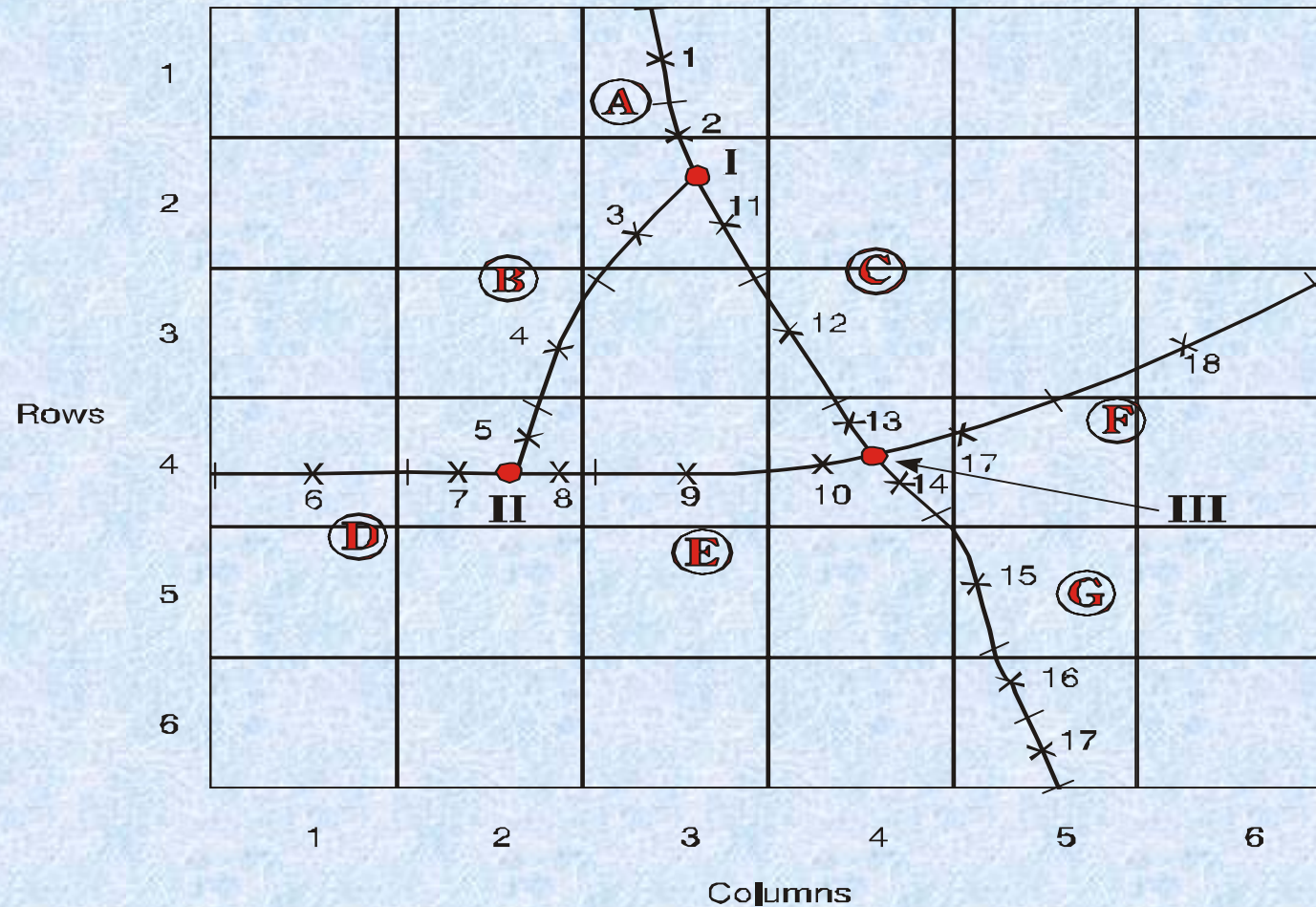
- At every stress period, the following may vary:
  - Boundary stresses
  - Evaporation rate
  - Friction coefficients along flow direction(s) for CHF /OLF
  - Rill height
  - Obstruction storage height
  - Reference ET input - or calculation parameters
    - Air density; atmospheric pressure; saturated vapor pressure; relative humidity; wind speed; temperature; radiation and soil heat adsorption; mean crop height; Monteith Canopy resistance parameters;
  - Leaf Area Index
  - Coefficients C1, C2, C3 for actual ET
  - Root zone distribution function
  - Crop Coefficient



# Discretization – Rectangular or Curvilinear Finite-Difference



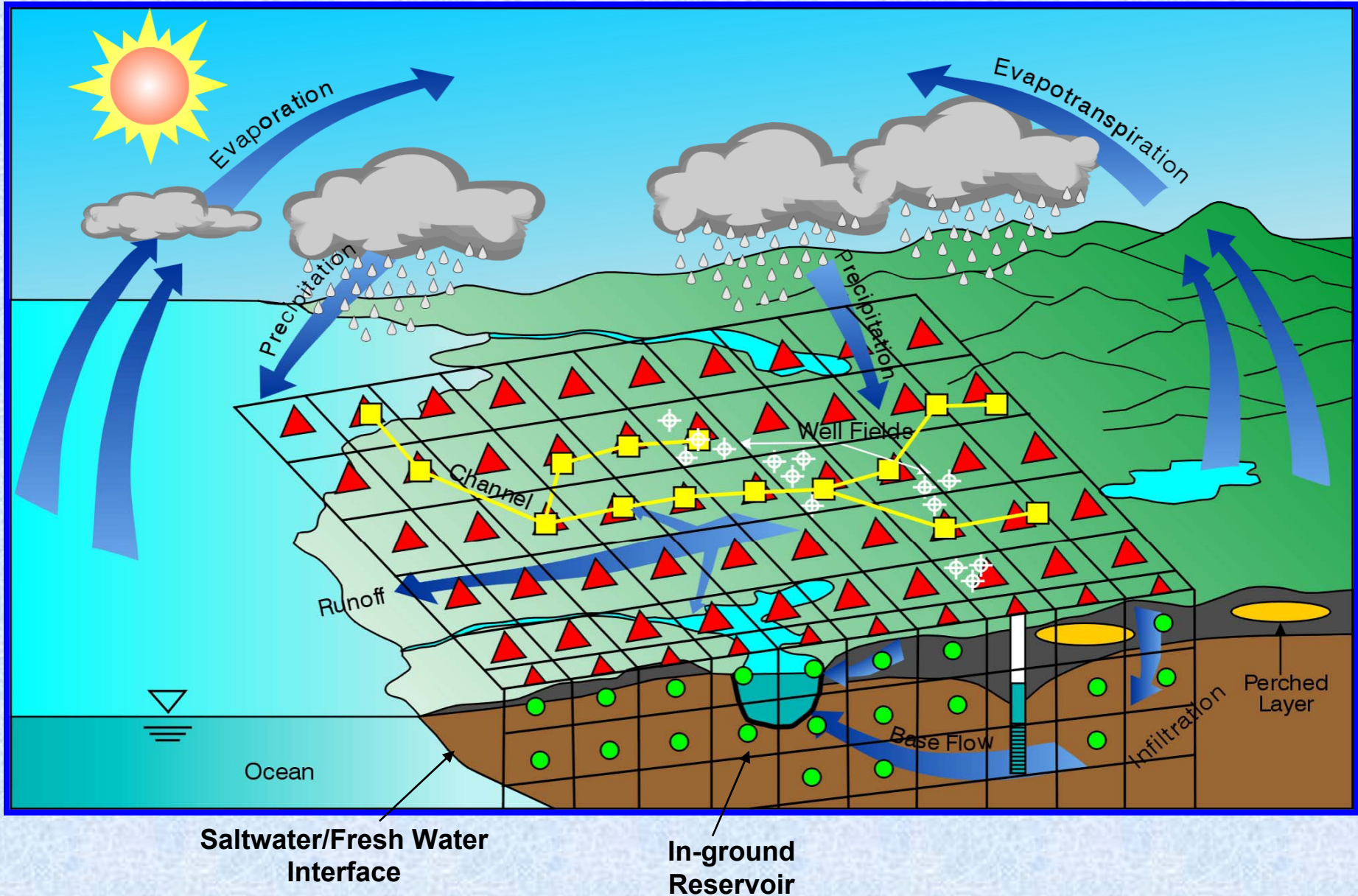
# Channel/Pipe Discretization – Finite Volume



—x— 1-D Channel Segment

● Junction

# Holistic Solution for Hydrologic Cycle

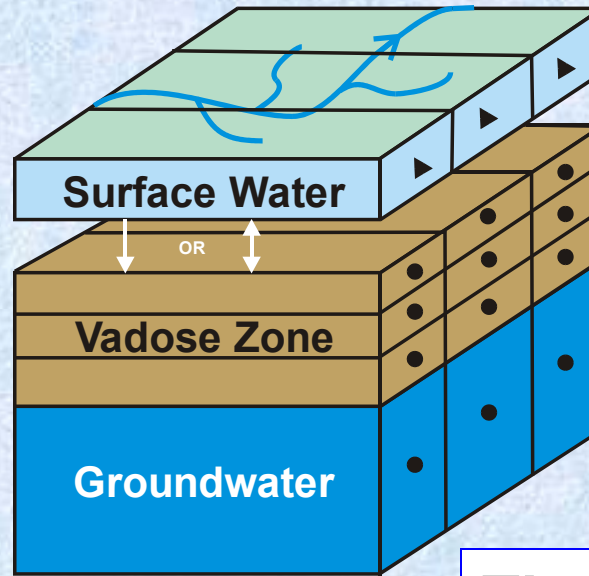
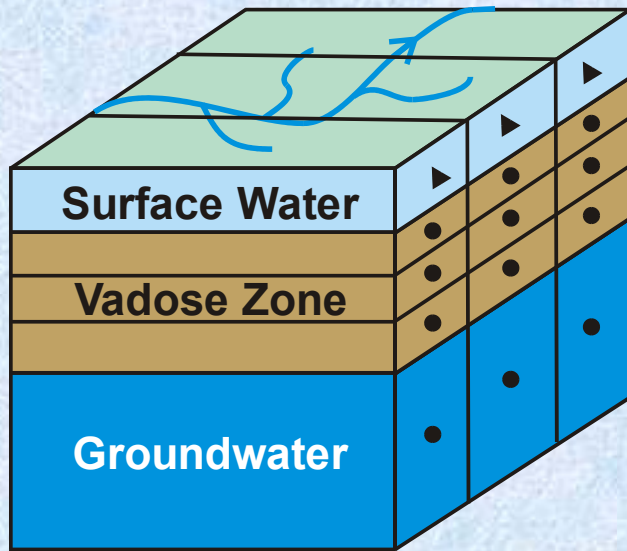


- Fully implicit, fully coupled solution with options for linked schemes
- Newton-Raphson Linearization available in addition to Picard option
- Unstructured Matrix Storage Scheme
- Orthomin, GMRES, BiCGSTAB Solution Schemes
- Adaptive Time-Stepping & Output Control
- Flexibility of conceptualization
  - **Parametric or Physics Based ET**
  - **Kostiakoff, Green Ampt, Richards Equation, GSVE**
  - **Mix-and-match of GW, OLF, CHF domains and boundary conditions**
  - **Node-Link method for conceptual models**



# Conjunctive Flow Solution Schemes

**Fully Coupled Solution:**      **Linked Solution:**

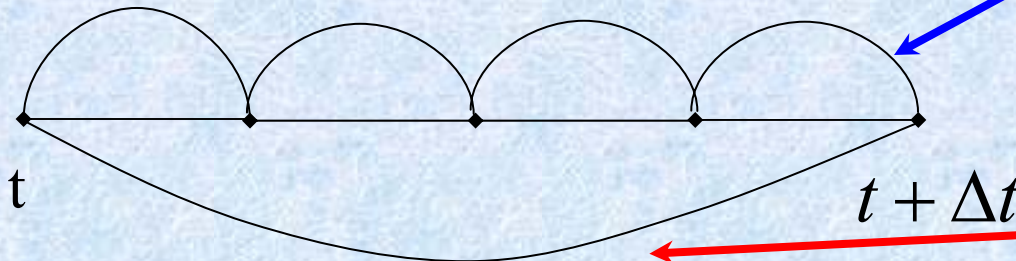


•Non-iterative

•Iterative

Coupling of Flux or Head at the Interface

**Time Stepping:**



Time steps for the surface water domain

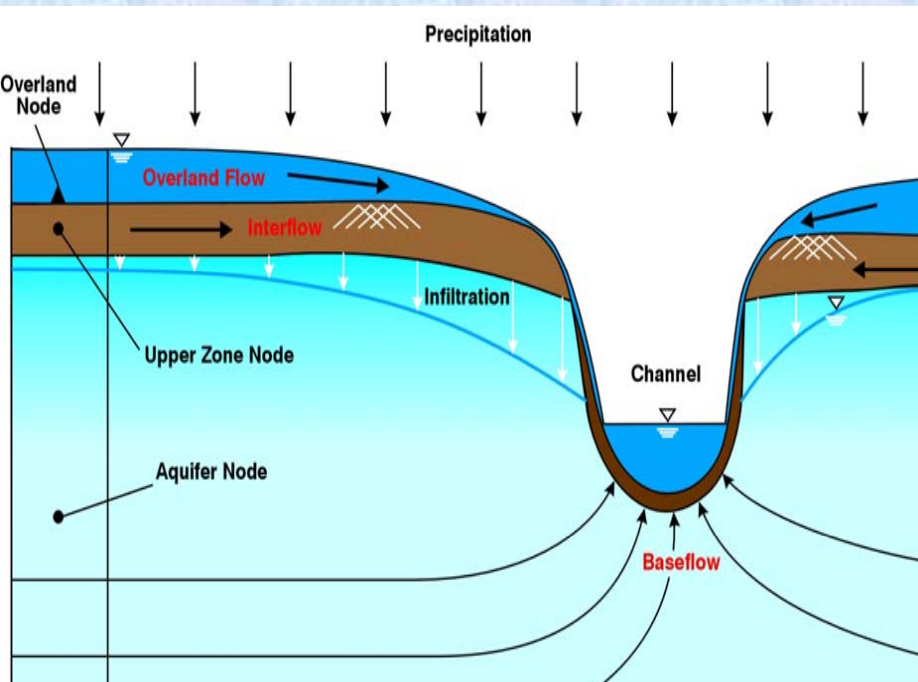
Time steps for the subsurface domain

# Comparison of Fully Coupled and Linked Schemes



- Fairbanks, et al., Comparison of Linked and Fully Coupled Approaches to Simulating Conjunctive Surface / Subsurface Flow and their Interactions – MODFLOW 2001 Conference
- Panday, Multi-Scale Conjunctive Modeling of Surface and Subsurface Flow – MODFLOW 2003 Conference
- Linked approaches give good results only for “small” time-steps

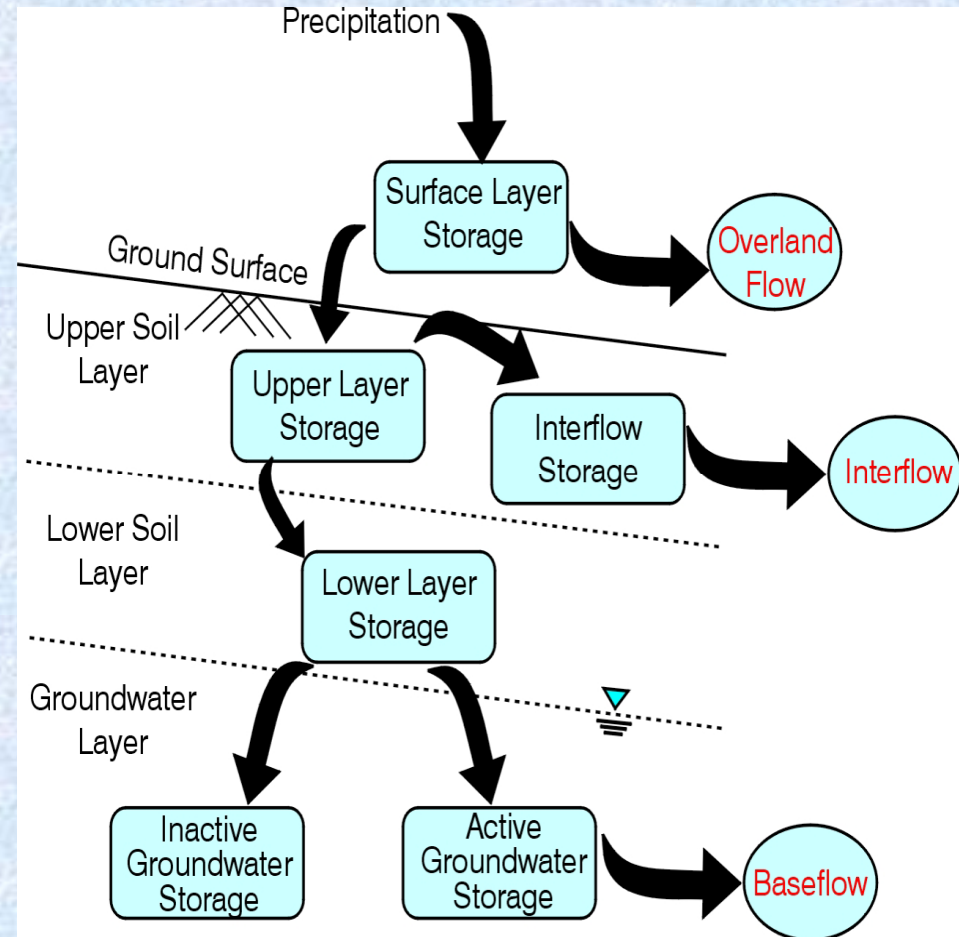
## Our Three-Layer Model Conceptualization



### Salient Features:

- Effective for regional and sub-regional applications
- Accounts for all components of the hydrograph including interflow
- Accurately track soil moisture storage, infiltration, and water table position

## Classical Conceptualization of HSPF (after Ford & Hamilton, 1996)



# Pre- and Post-Processing

- ViewHMS provides complete pre- and post-processing capabilities
  - **Create / modify grids, assign properties and boundary conditions manually or automatically**
  - **Import Shape-Files with various interpolation options to parameterize spatially varying properties**
  - **Query Access Databases for hydraulics**
  - **Manipulate input and output data for calibration, and calibration statistics**
  - **Read model output files for viewing / export to Tecplot, Surfer/Grapher, ArcGIS, Maya, Modflow Binary**



## Pre- and Post-Processing - Continued

- ArcHMS plug-in for ArcGIS provides direct interface of ArcGIS to model files
- Subsurface setup in any MODFLOW processor
- Fully documented ASCII input files allow manual editing for minor changes, QA, or user development of pre-processing utilities
- Standard ASCII and binary output files based on MODFLOW format. This allows user development of customized post-processing utilities for interfacing with software of choice

# Summary of Model Formulation

- Basin Hydrology – 2-D spatially distributed
- Initial abstractions – Detention storage; Infiltration; Interception; ET
- Infiltration options – GSVE; Richards Equation; analytic infiltration formulas
- SW-GW Interaction – Holistic; fully coupled; mass conserved (adaptive time-steps); drying of rills provides converged solutions
- GW interactions between sub-basins – Solves GW flow rigorously
- Detention Storage – Estimated for rills; Includes obstruction storage exclusion

# Summary of Model Formulation - Continued

- Runoff generation – Diffusive wave; User defined (tabulated)  $Q-h$  (or  $Q-h^1h^2$ ) via Node-Link method
- Hydrologic routing – Holistic, physics-based, spatially-distributed; Node-Link method
- Hydraulic routing – Various canal cross-sections; Node-Link method
- Hydraulic structures – Various options of tabulated input (ViewHMS provides formulas)
- Structure operations – Comprehensive
- Screening mode – Flexible domain options; Node-Link method; infiltration options; ET options; adaptable boundary conditions



# Summary of Model Formulation - Continued

- Groundwater hydraulics
  - Finite-difference / Finite-volume combination;  
Rectangular / Curvilinear Grids
  - Quasi-3D and fully 3-D setups within the same simulation
  - Saturated / unsaturated zone solved fully 3-D holistically
- Adaptive time-stepping to assure convergence within and among all domains
- Flexibility of formulations and boundary conditions to suit problem objectives and available data
- Holistic hydrologic cycle simulation with linked alternatives in an adaptive time-stepping framework



# Specifics of SW-GW Interaction Implementation

- Linkage between GW and SW grids: canals, wetlands, sub-basins, infiltration, exfiltration etc. – Fully coupled: GW and SW interaction based on Darcy's Law; SW interactions based on weir equations
- Features at a smaller scale than model grid – Finite-Volume connectivity; node-link approach
- Secondary or Tertiary Canals Interaction with GW – Holistic, physics-based interactions between all connectivities
- Reservoir Routing and hydraulic routing problems at C&SF structures – Includes high level of complexity

# Flood Routing Problems of Kissimmee Basin

- Characterize regional hydrology, calculate lake stages, river flows, discharge from KB into Lake Okeechobee, effects of water control structure operations, impacts of Floridan Aquifer pumping – Holistic, comprehensive and rigorous SW\_GW modeling capability with structures and operations
- Long term simulation (20 to 30 years) and flood event simulation (days) – Adaptive time stepping
- Local and regional levels of resolution – multi-scale features; node-link approach

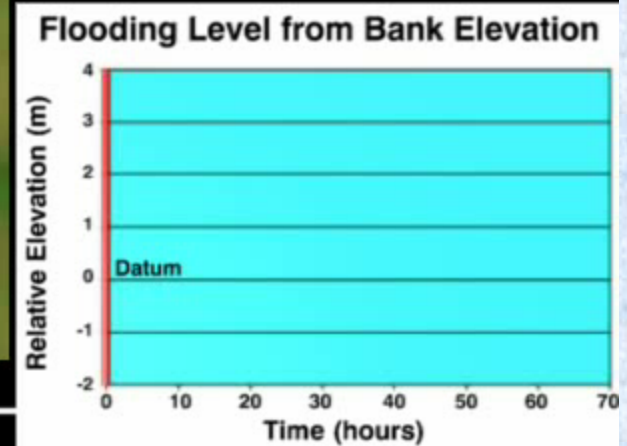
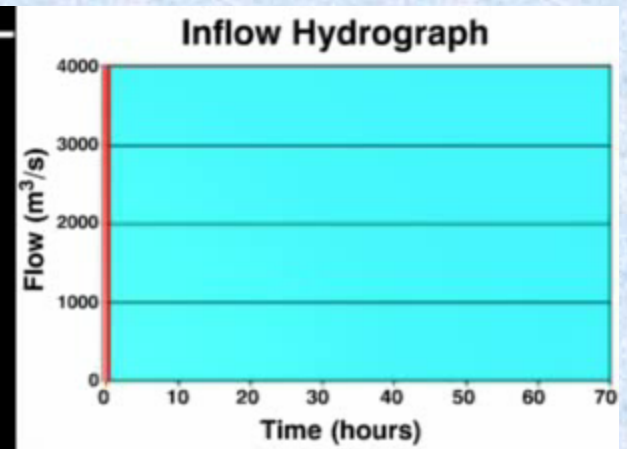
# Flood Routing Problems of Kissimmee Basin – continued

- Address Uncontrolled / Controlled and Free / Submerged combinations of gate opening and tailwater submergence – Combinations of Structures and Operations
- Incorporate effects of urbanization trends – Temporal input of land use related properties, canal properties, or canal existence
- Address phosphorous reduction strategies – Comprehensive reactive transport simulation capabilities

# Flood Routing Problems of Kissimmee Basin – continued

- Perform screening level investigations –  
Flexibility to suit problem and available data
- Comprehend results and convey them to  
reviewers, stakeholders and decision makers –  
Output can be processed for a variety of tools  
for analysis and visualization





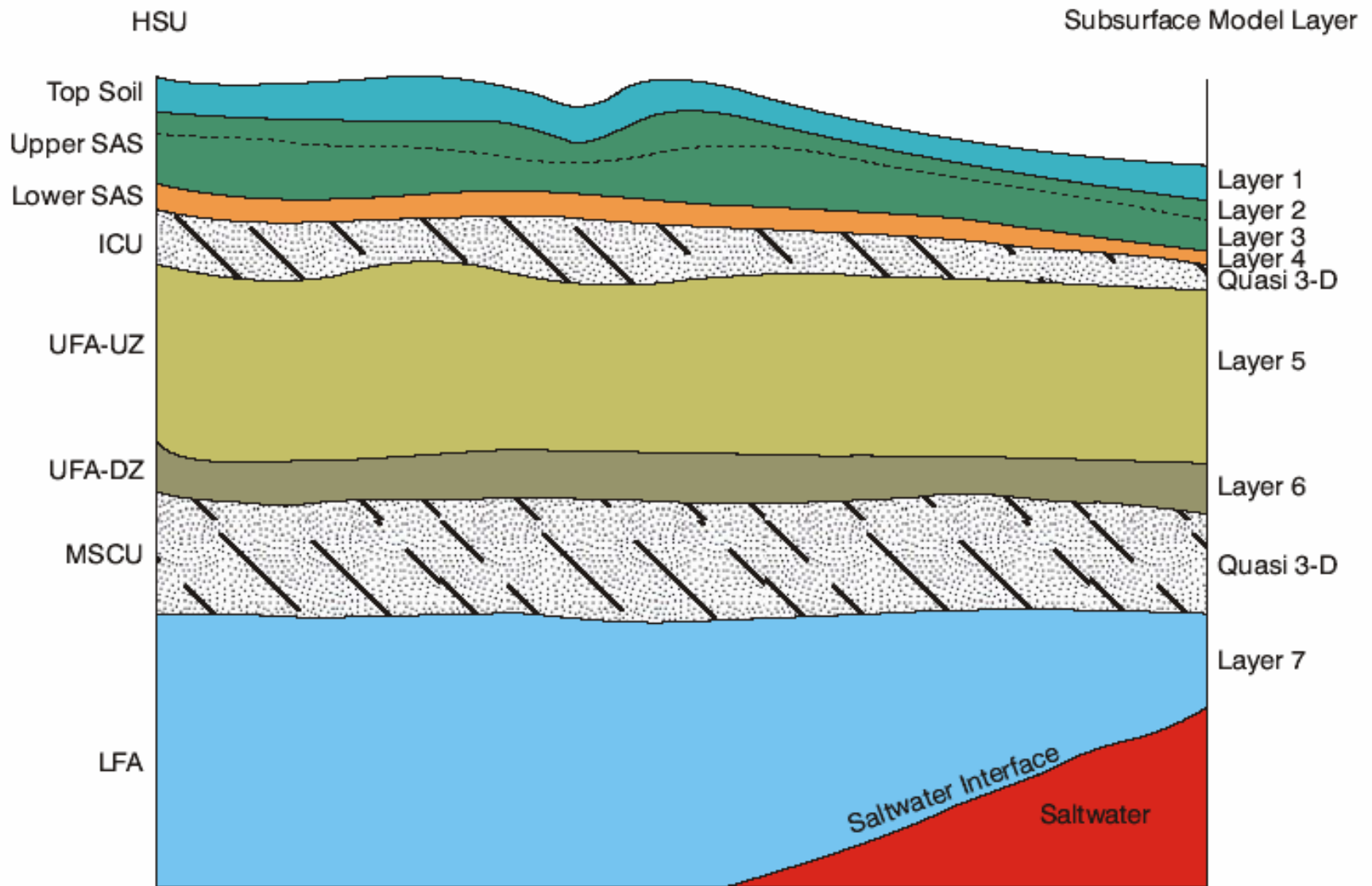
# MODHMS Application Example – WOSC-ISGM around Orlando, Florida

- Regional ECF groundwater flow model – **Used for Water Supply Permitting**
- Surface-water features are inter-connected or internally drained – **Highly Engineered System**
- Conjunctive model was needed to assess overall water management, recharge, and impact of FAS withdrawals on surface water bodies
- ECF groundwater model was conceptualized via lumped estimates of hydrologic cycle components

# WOSC-ISGM Setup and approach

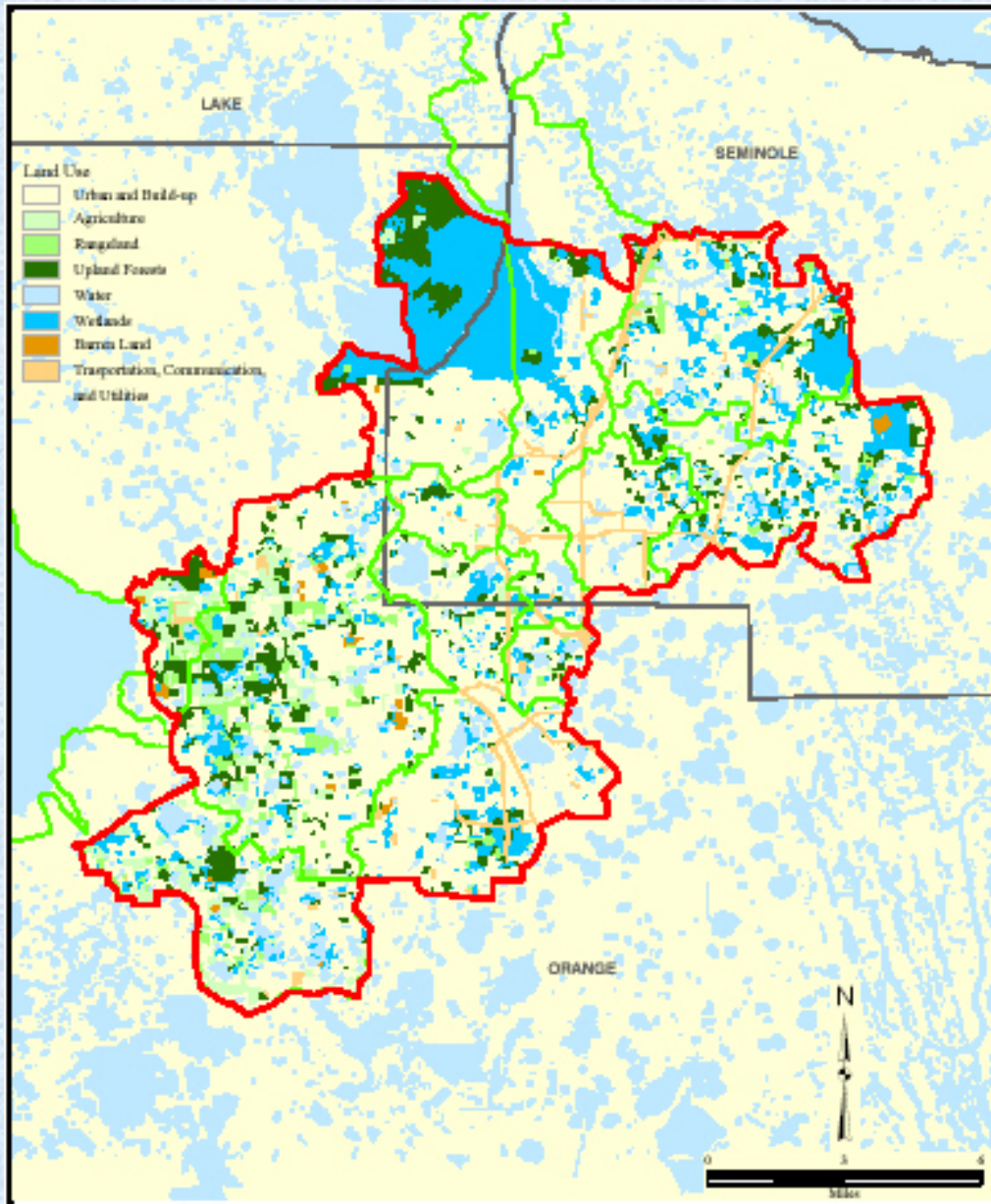
- WOSC-ISGM expands on flow model conceptualization of ECF model
- Telescope from regional ECF model and include complexities of SAS, surface hydrology & hydraulics
- Grid-size 625 ft areally
- Around 180,000 active nodes
- Model includes 3-D unsaturated zone, physics-based ET, detailed hydraulics and drainage wells (node-link)
- Model implementation performed in 18 months

# Subsurface Conceptualization





# Model domain and parameterization



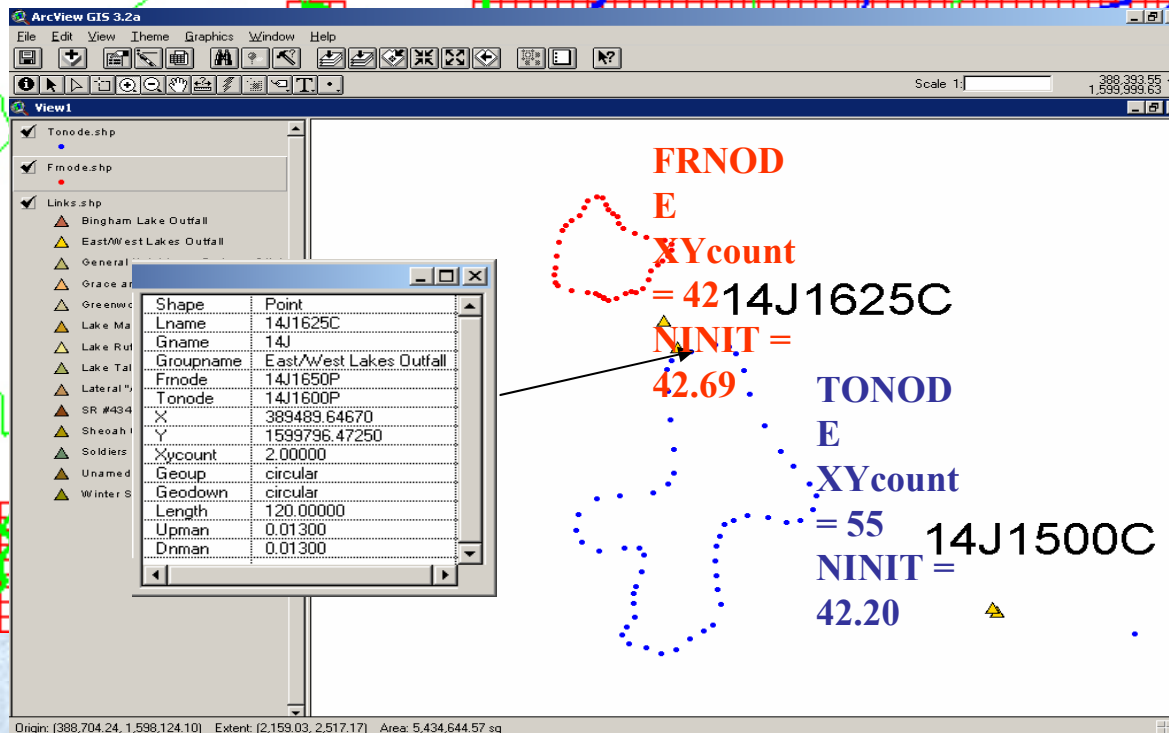
- **Land-Use / Land Cover:** LAI, friction, RDFI, EDFI, Surface Leakance
- **Soils Data:** Moisture retention, porosity, conductivity, field-capacity and wilting-point saturations

# Other Parameterization and Input

- **Geology and Stratigraphy:** Aquifer characterization
- **DEM:** Surface elevation
- **Hydrology Databases:** Drainage system geometry, connectivity and characteristics, Surface-water body features, and Structure characteristics and operations
- **NEXRAD data:** Precipitation
- **Well permitting databases:** Withdrawal estimates
- **Various GIS coverages:** Local water budget components, agricultural or septic water returns, domestic well withdrawals, Land-Use changes, etc.



# Hydrology from ICPR databases



FRNOD

E

XYcount

= 42 14J1625C

NINIT =

42.69

TONOD

E

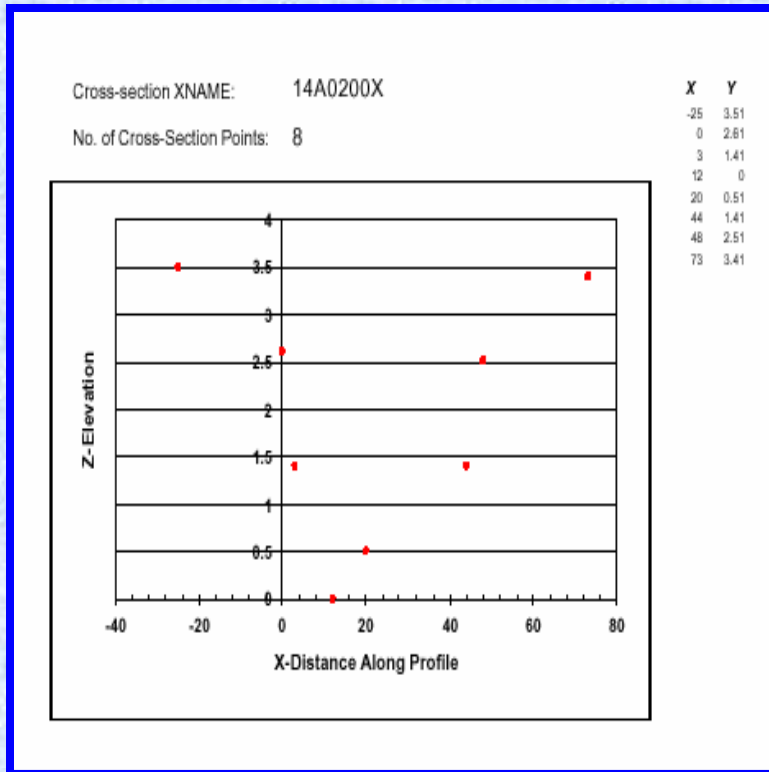
XYcount

= 55

NINIT =

42.20

14J1500C



Microsoft Access - [ICPR\_\_\_B : Table]

	NNAME	XVAL	YVAL	ZHANDLE
▶	WOODLAND	85	19.05	-1
	WOODLAND	80	2.87	-1
	WOODLAND	76	1.05840747	-1
	WOODLAND	75	0.91358231	-1
	WOODLAND	74.5	0.73969647	-1
	WOODLAND	73	0.7	-1
	WOODLAND	8	0	-1
	WINSOR	87	26.3808224	-1
	WINSOR	86	22.5119142	-1
	WINSOR	85	21.59972833	-1
	WINSOR	84	20.88222973	-1
	WINSOR	83	20.18237603	-1
	WINSOR	82.7	19.5979562	-1
	WINSOR	11	0	-1
	WEST	70	43.37475481	-1
	WEST	69	41.62717461	-1
	WEST	68	39.81007518	-1

The model was assembled and calibrated to average 1995 conditions and to transient conditions from June 1995 through September 1999 (June 1997 onwards used for verification)



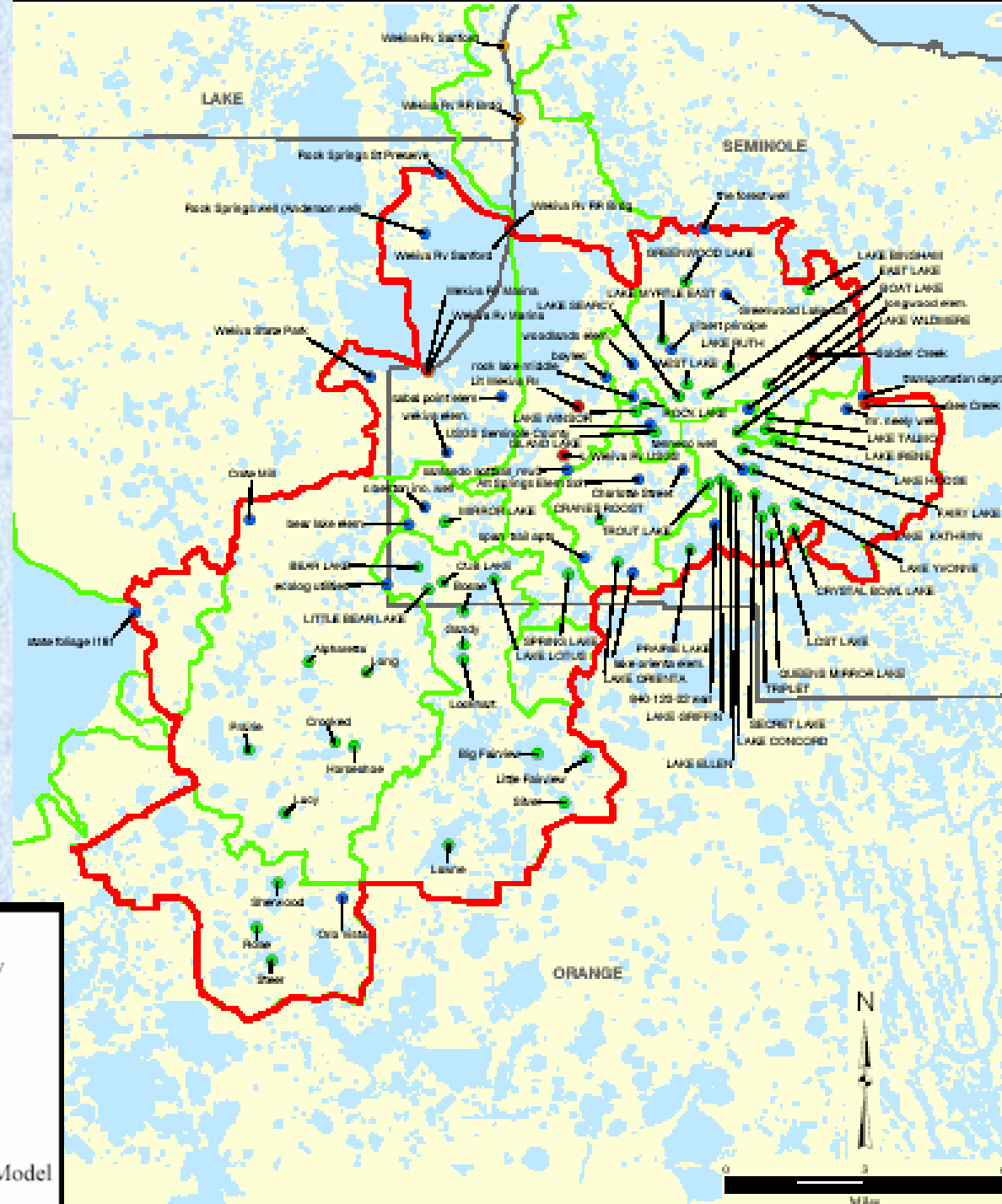
# Observation Locations

## 1-36 Subsurface (36)

## 37-87 Lake Stage (51)

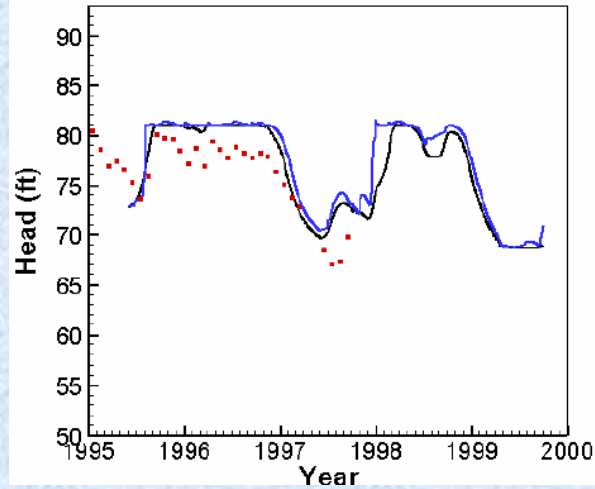
## 88 Spring Flux (1)

## 89-96 Stream Flow (8)

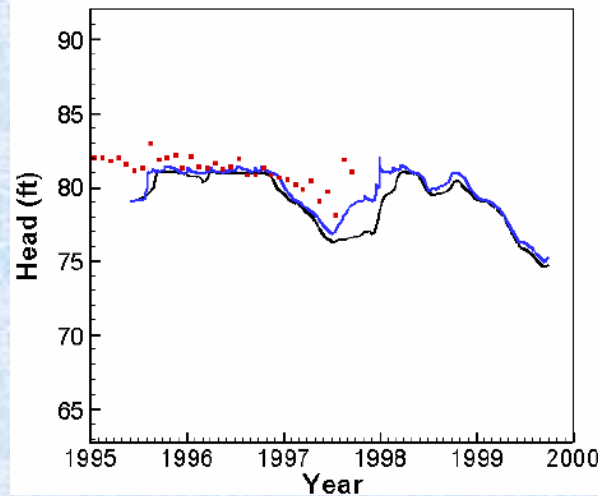


# Results for Daily vs. Monthly Rainfall

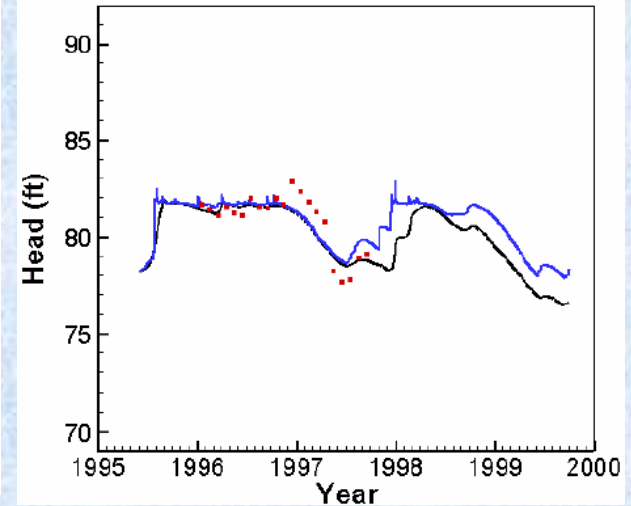
• Observation 85 at Sherwood



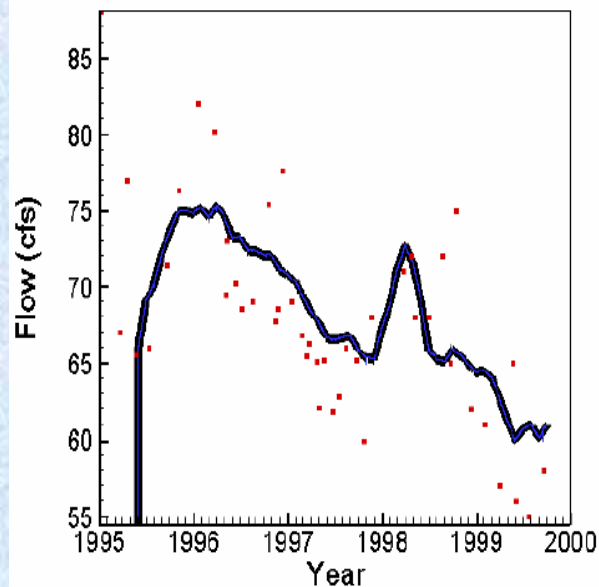
• Observation 86 at Rose



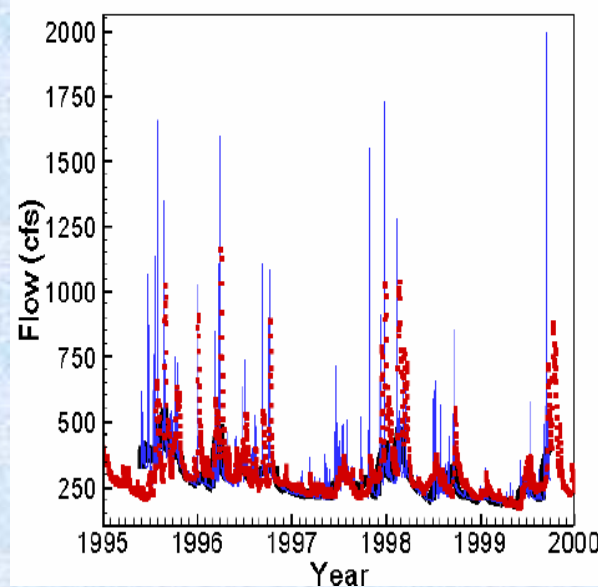
• Observation 87 at Steer



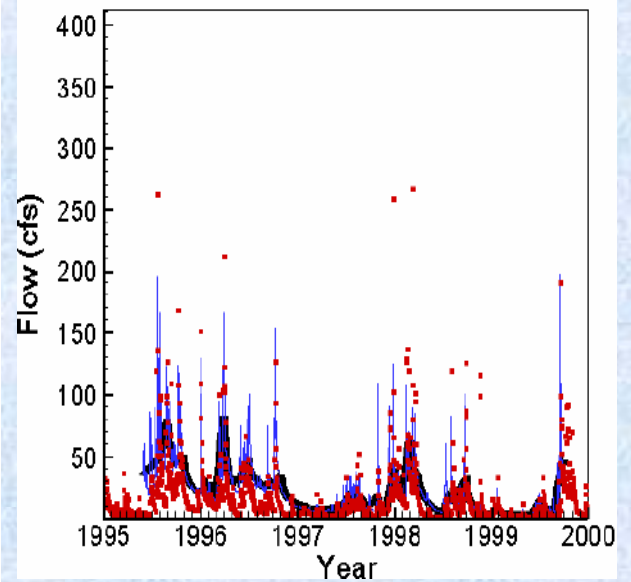
• Observation 88 at Wekiva spring



• Observation 90 at Wekiva R v Sanford

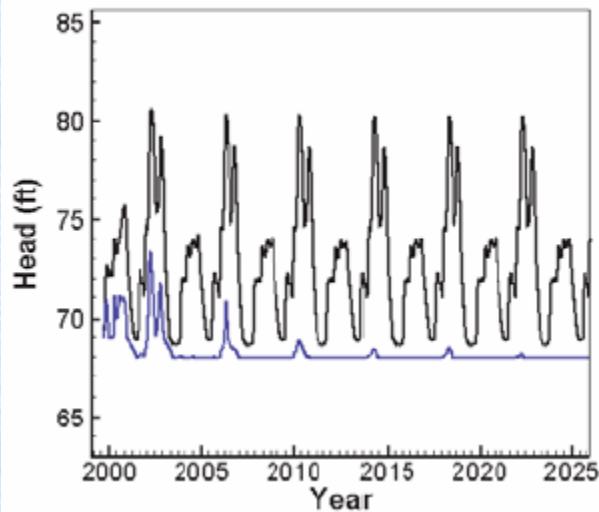


• Observation 92 at Soldier Creek

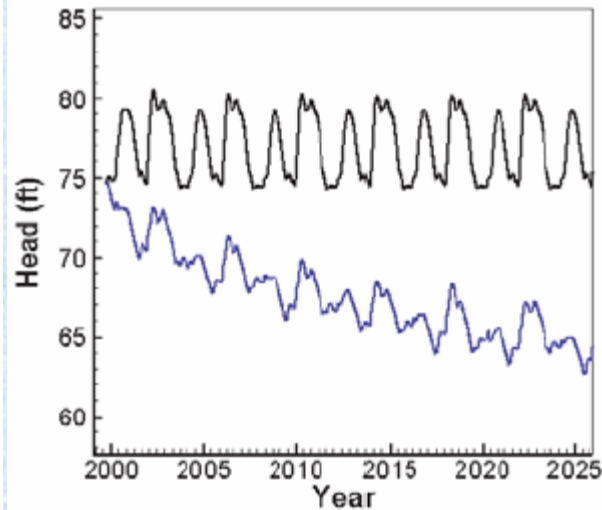


# Results for Higher Floridan Pumping

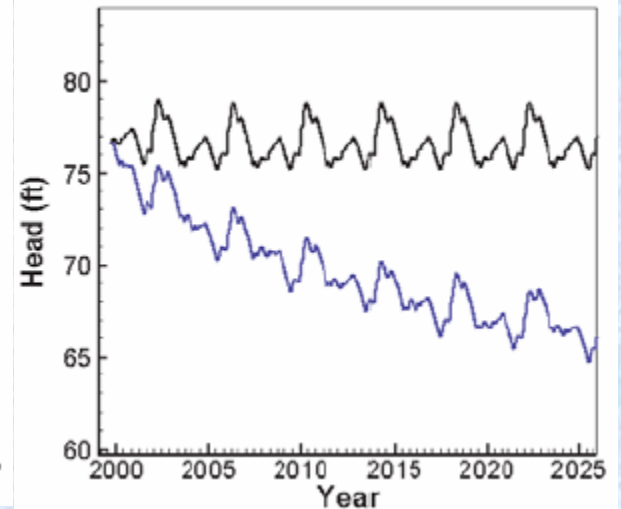
• Observation 85 at Sherwood



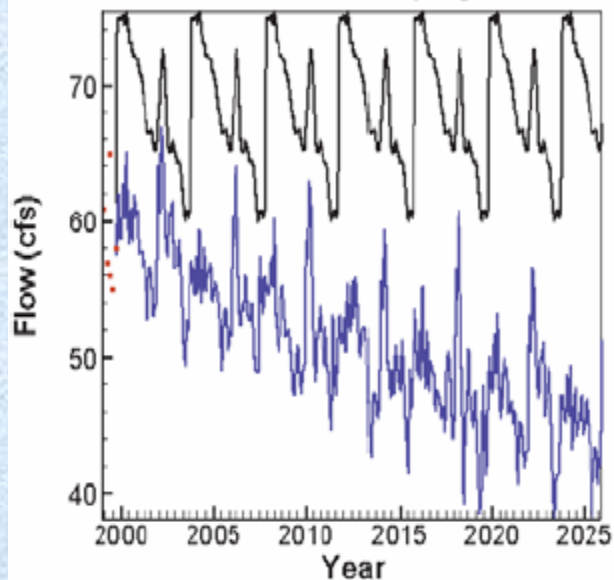
• Observation 86 at Rose



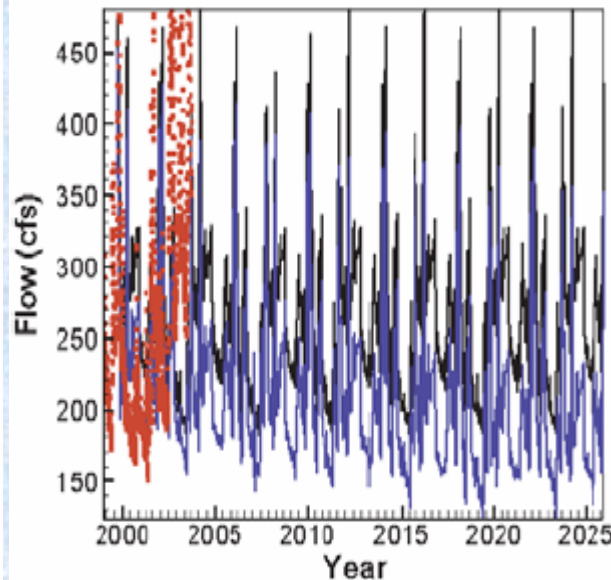
• Observation 87 at Steer



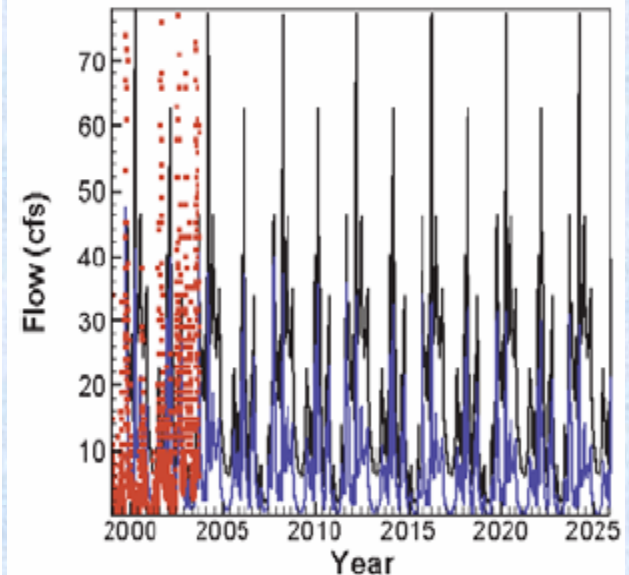
• Observation 88 at Wekiva spring



• Observation 90 at Wekiva Rv Sanford



• Observation 92 at Soldier Creek



# Computation Run-times – On Pentium IV, 2000 MHz

- June 1995 through September 1999 with daily precipitation fluctuation – 14 days
- June 1995 through September 1999 with monthly averaged precipitation fluctuation – 3 days
- September 1999 through September 2025 with monthly averaged precipitation fluctuation – 16 days
- NOTE: Today's Pentium machines are at least twice as fast.
- NOTE: Richard's Equation solution (and to some degree physics based ET) provide greatest numerical difficulties



# Strengths vs weaknesses for potential KB application

- Holistic approach for multi-scale objectives
- Incorporates general structures and rules of operation
- Flexibility of formulation to adapt to problem objectives and available data
- Adaptive time-stepping for large rapid events
- Rigorous formulation that does not ignore convergence of simulation between domains
- Complex data processing and manipulation
- Diffusion wave neglects inertial effects

# Proposed model implementation strategy for the Kissimmee Basin

# Data Needs

- Elevation data
- Rainfall data
- LAI, RD,  $ET_p$
- USGS NED or higher resolution project data if available
- Can use NEXRAD data or SFWMD data and Thiessen polygon or SFWMD TIN approach
- Can use existing MIKE SHE database, USGS data, SFWMD data, and/or literature values

# Data Needs

- Overland roughness coefficients
- Canal Cross-sections
- Canal roughness coefficients
- SFWMD land-use based Manning's data
- Can use available HEC-RAS and MIKE 11 cross-sections
- Can use values from calibrated HEC-RAS, MIKE 11, and AdICPR models or literature values



# Data Needs

- Canal network
- Structure protocols
- Canal boundary conditions
- Can use available existing HEC-RAS, MIKE 11, and AdICPR networks and GIS coverages (ArcHMS)
- Can use logic in existing HEC-RAS, MIKE 11, and AdICPR files and SFWMD/USACE rules
- Use available data from DBHYDRO

# Data Needs

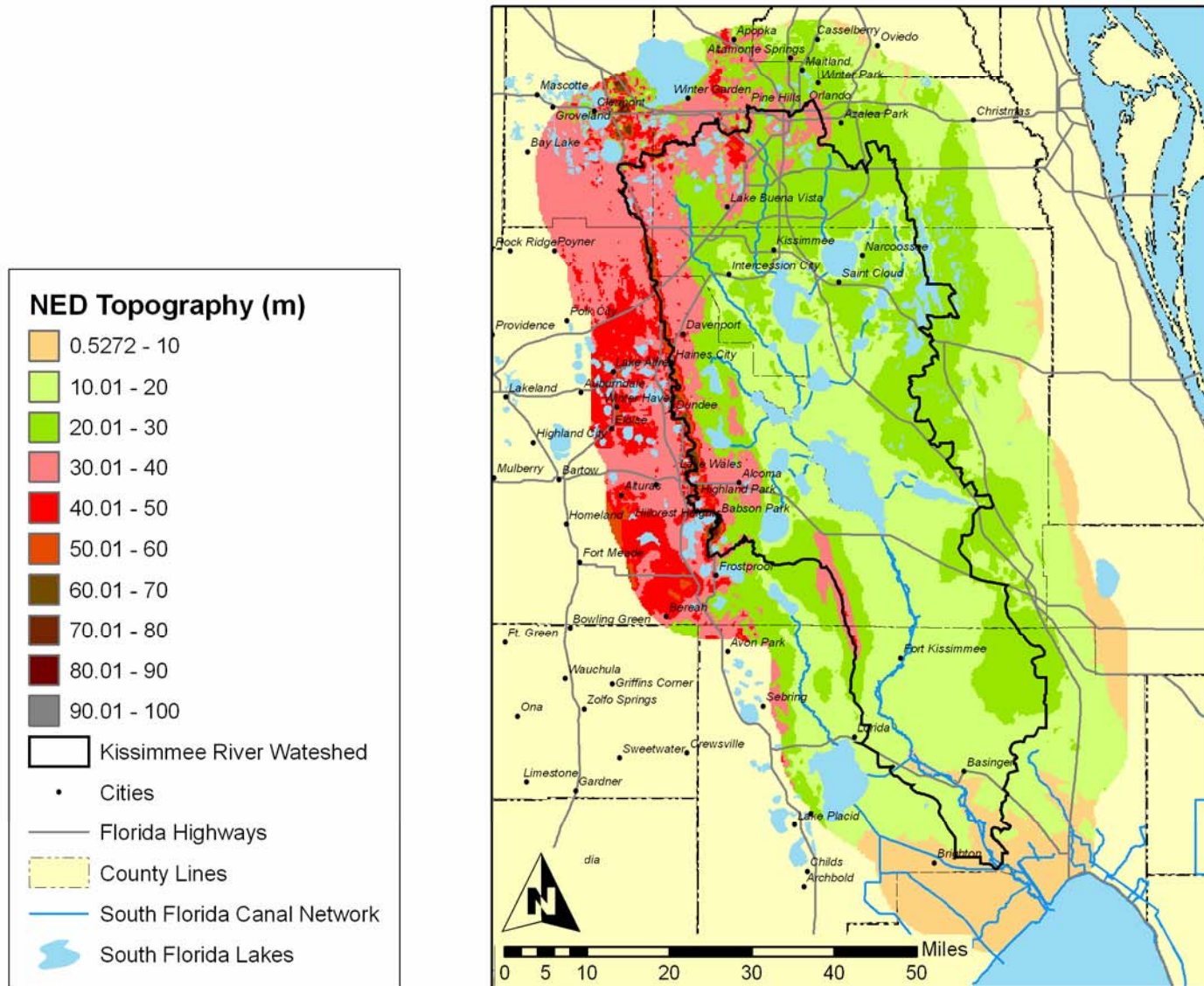
- Unsaturated Hydraulic Parameters
- Hydrostratigraphy
- Saturated Hydraulic Parameters
- Representation of sinkholes
- Can use existing MIKE SHE database or UofF Soil Database if solving Richard's Equation
- Can use data from existing MODFLOW and MIKE SHE models, USGS studies, SFWMD studies, and any available county studies.
- Can use existing MIKE SHE and MODFLOW files and available surficial aquifer data
- Can rely on available understanding of connection of karst features with the SAS, ICU, and FAS

# Data Needs

- Saturated Zone Boundary Conditions
- Saturated Zone Pumping Rates
- Canal Abstractions (if present)
- Irrigation areas, rates, etc.
- Can use no-flow for surficial aquifer at surface water basin boundary
- Can use available SFWMD data
- Can use available SFWMD data
- Can use available SFWMD data and MIKE SHE irrigation database and results

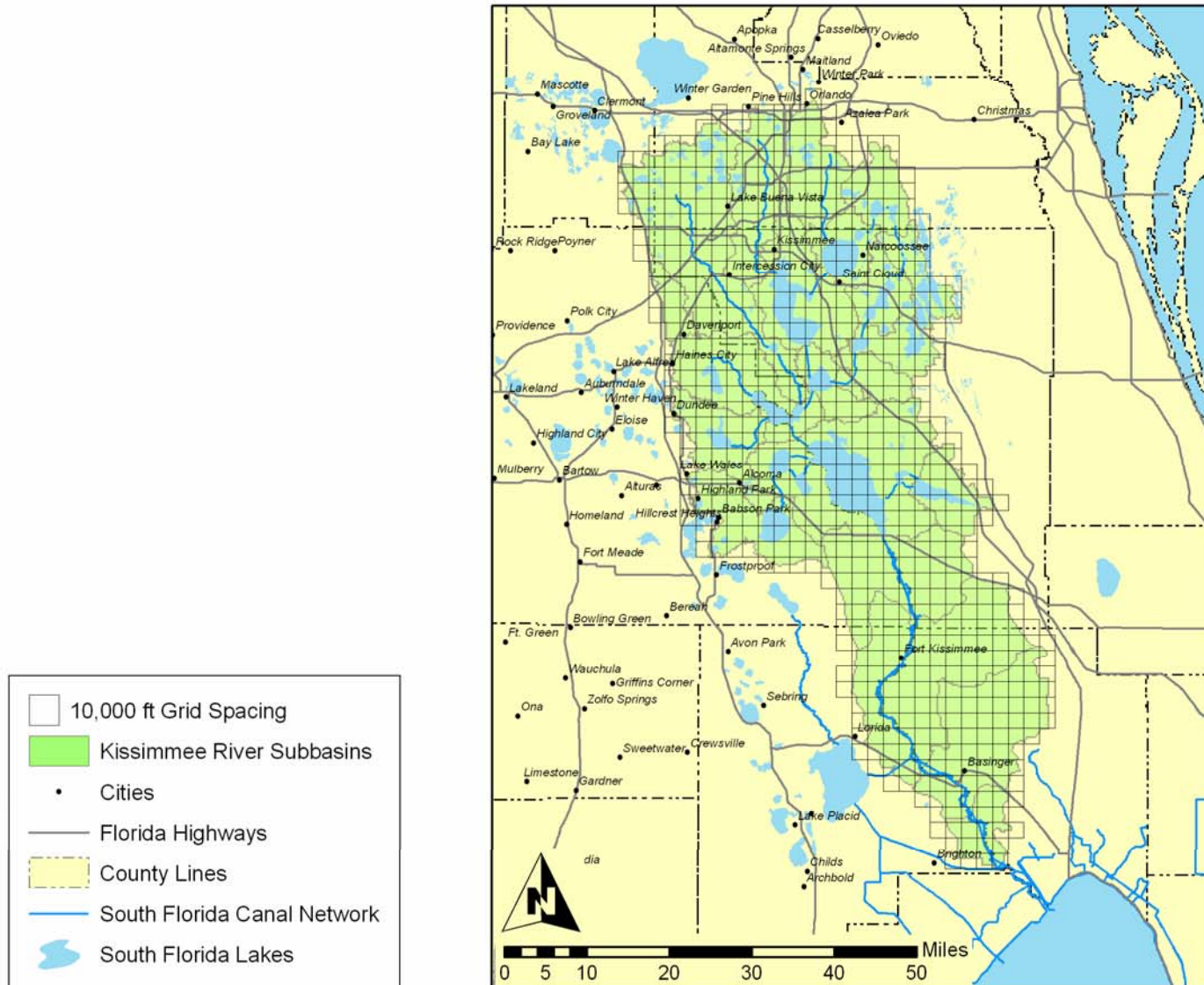


# Basin Delineation





# Grid Size



# Discretization Assumptions for run-time calculations

- Unsaturated Zone response needs to be explicitly modeled using the Richard's equation formulation
- The Floridan aquifer system can be modeled as a simple head-dependent flux boundary condition

# Grid Size

<b>Grid Size (ft)</b>	<b>No. Columns</b>	<b>No. Rows</b>	<b>No. Active Cells</b>
500	~ 550	~986	~252,636
1000	275	493	63,159
2000	~ 138	~ 247	~15,790
5000	~ 55	~ 99	~2,527

# Example Run Times

<b>Model</b>	<b>Notes</b>	<b>No. Active Cells</b>	<b>CPU Speed</b>	<b>Approximate Run Time (hrs/yr)</b>
Mobile Bay	Pseudo soil functions, very detailed		~1 GHz	55
WOSC	Richard's Equations, daily rainfall	~180,000	~2 GHz	78
WOSC	Richard's Equations, avg. monthly rainfall	~180,000	~2 GHz	17
WOSC	Richard's Equations, avg. monthly rainfall	~180,000	~2 GHz	15



# Estimated Run Times

<b>Grid Size (ft)</b>	<b>Col, Row, Layers</b>	<b>No. Active Cells</b>	<b>Approximate Run Time (hrs/yr) 3 GHz</b>
500	~ 550, 986, 4 (+1 OL)	~1,263,180	~76
1000	275, 493, 4 (+1 OL)	315,795	19
2000	~ 138, 247, 4 (+1 OL)	~78,950	~5
5000	~ 55, 99, 4 (+1 OL)	~12,635	~1

# Model development and calibration

<b>Task</b>	<b>Conceptual Models</b>	<b>Detailed Models</b>
Data assimilation/ model development	2 weeks to several months	3 to 4 months
Calibration	weeks to months	3 to 4 months
Scenarios	days	days to weeks

# Optimization

- Non-proprietary input and output files permit interfacing with PEST for parameter estimation, sensitivity analyses, uncertainty analyses, and optimization
  - *A interface between MODHMS and stand-alone optimization package was developed for SJRWMD*
  - *UCODE or PEST could be used to optimize operation rules for KRB*

# Conclusions

- MODHMS has been successfully applied in similar regions of Florida
- MODHMS could be applied to the KRB in conceptual and detailed applications
- MODHMS has a rich set of options that would allow the model development to be tailored to the problem and aggressive project schedule
- MODHMS can deal with rainfall, ET, runoff, canal-aquifer interactions, surface-subsurface exchange, and flooding in a natural manner using a mass-conservative physics-based approach



# Conclusions

- The level of detail in the detailed model(s) must be consistent with the project schedule and may require an iterative approach during model development
- Recommend applying MODHMS using the psuedo-soil functions
- Recommend calibrating the detailed model(s) using a coarse discretization ( $\geq 2000$  ft) and using a final discretization of  $\sim 1,000$  ft
- It may be possible to use PEST or UCODE to optimize KRB operation/management rules (the non-proprietary format will facilitate this)

# Discussion